

Historic, Archive Document

Do not assume content reflects current scientific knowledge, policies, or practices.

Reserve

25591

A222

U. S. DEPT. OF AGRICULTURE
NATIONAL AGRICULTURAL LIBRARY

United States Department of Agriculture
Soil Conservation Service
Engineering Division

MAR 26 1973

CATALOGING - PREP.

Technical Release No. 33
Hydrology Branch
August 1966

SIMPLIFIED METHOD FOR DETERMINING FLOODWATER RETARDING STORAGE

The procedure is an approximation for determining the minimum required floodwater retarding storage for single-stage principal spillway structures. It will apply where there is reasonable assurance that a single-stage is more economical than an equally effective two-stage principal spillway. The method is based on use of the principal spillway mass curves (PSMC) included in Chapter 21 of the National Engineering Handbook, Section 4 - Hydrology, issued in August 1965. The method is useful for estimating the minimum storage requirement for floodwater retarding structures in which the release rate and 10-day runoff are within the limits of the accompanying graphs (Figures 1 through 8) and the structure complies with the following provisions:

- a. The structure has a single-stage principal spillway;
- b. That on (shallow) reservoirs with gently sloping topography, where storage increases greatly with small increases in stage, this procedure may underestimate the required retarding storage volume. In this situation the PSMC should be routed;
- c. That the release rate and 10-day runoff (Q_{10}) to be used with the graphs are based on the procedure in Chapter 21, NEH 4 (accounting for base flow, snowmelt and channel losses);
- d. That the release in Figures 1 through 8 is further considered as a new rate, excluding the release from upstream structures in series.

The attached curves eliminate the necessity of plotting the PSMC. The runoff volumes at 1 day (Q_1) and at 10 days (Q_{10}) are determined and the ratio of Q_1/Q_{10} is computed. This ratio and a selected average release rate through the principal spillway are used with Figures 1 through 8 to determine the minimum retarding storage requirements.

This simplified procedure is illustrated by its application to Examples 21.1 and 21.2 in Chapter 21.

Example 21.1 (page 21.10 of Chapter 21). In this situation, the climatic index is less than 1.00 and channel losses are considered.

1. Estimate the direct runoff for 1 and 10 days. This was determined to be $Q_1 = 4.37$ and $Q_{10} = 6.34$ inches.

2. Compute the climatic index. In the example $C_i = 0.603$.
3. Estimate the net runoff. For the climatic index and drainage area size, the reduction factor is 0.75. Multiply Q_1 and Q_{10} of step 1 by this factor to get net runoffs of 3.28 and 4.76 inches respectively.
4. Compute the Q_1/Q_{10} ratio. From step 3, $Q_1/Q_{10} = 3.28/4.76 = 0.69$.
5. Select an average release rate through the principal spillway. The maximum release rate through the principal spillway is 150 c.f.s. which represents 10 c.s.m. for the 15 square mile drainage area. The average release rate for a single-stage structure was estimated to be 70 percent of this rate, or 7 c.s.m.
6. Determine minimum floodwater retarding storage. Use Figure 6, attached, for the closest Q_1/Q_{10} ratio of 0.70 and the applicable T_c value of 7.1 hours. Note that Figure 6 covers a range in T_c from 0.1 to 9.0 hours. With a Q_{10} runoff of 4.76 inches and an average release rate of 7 c.s.m. the floodwater retarding storage is 3.15 inches.

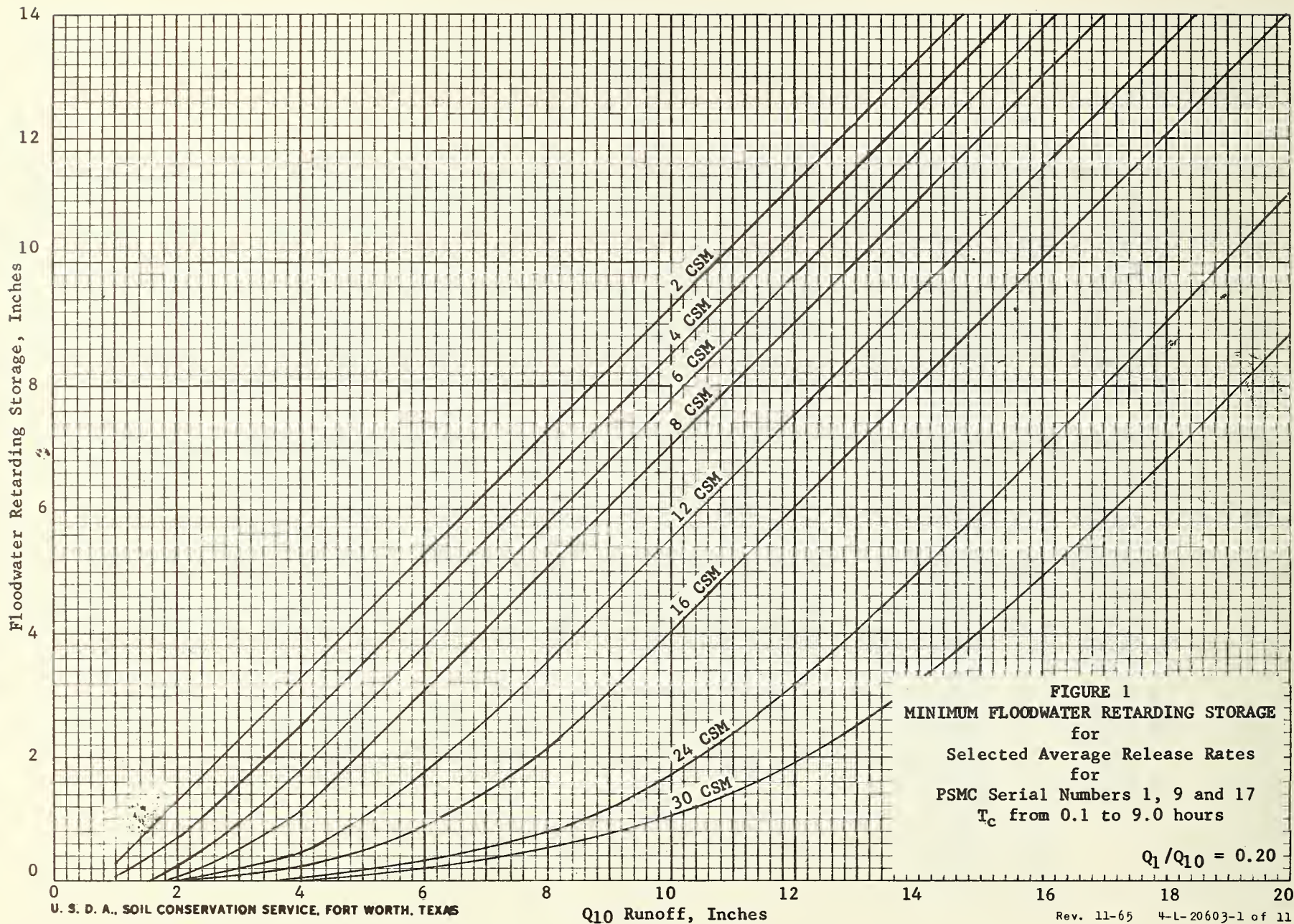
Example 21.2 (page 21.14 of Chapter 21). In this situation, the climatic index is greater than 1.00, and the addition of base flow is to be considered.

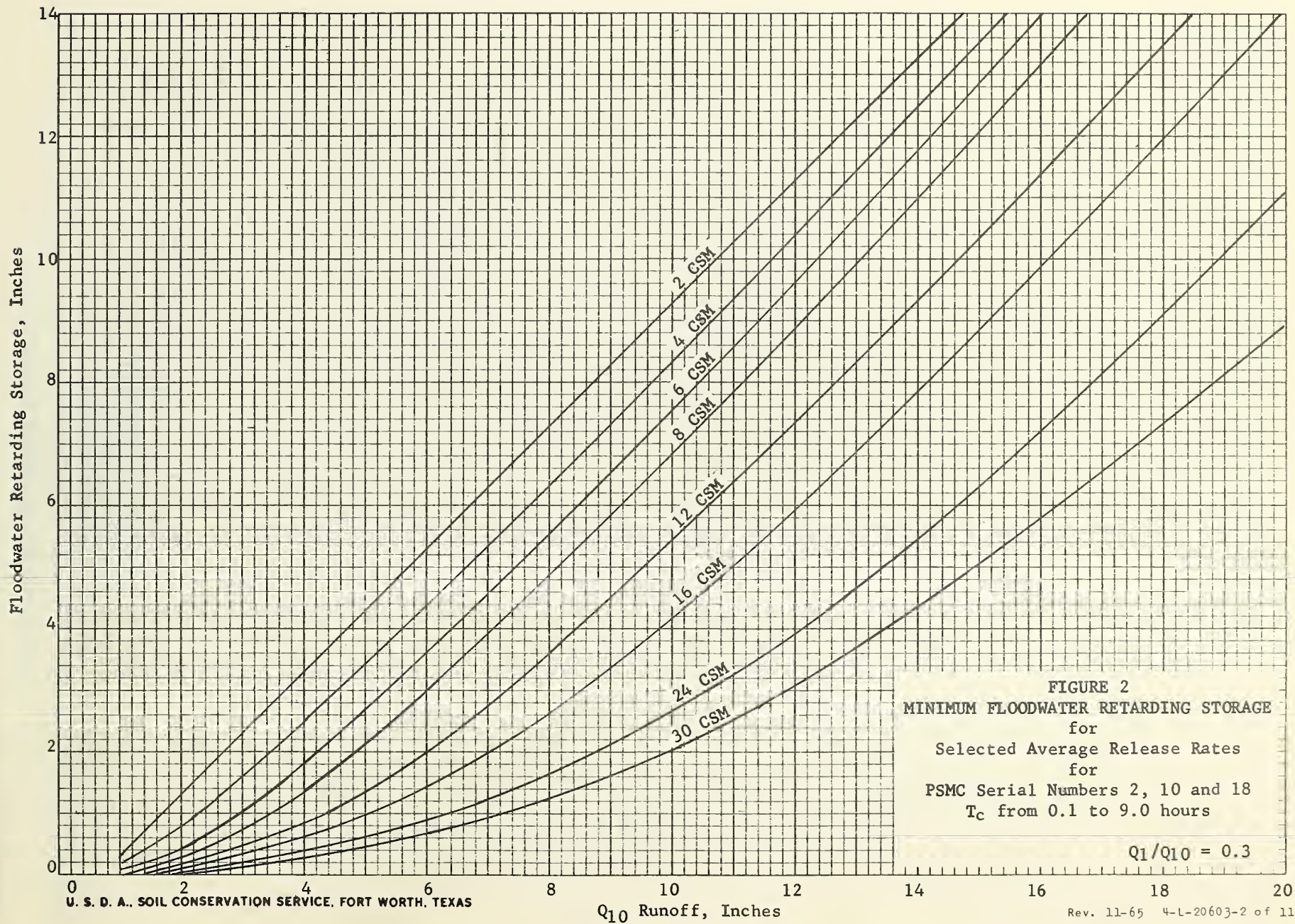
1. Estimate the direct runoff for 1 and 10 days. This was determined to be $Q_1 = 2.94$ and $Q_{10} = 6.68$ inches.
2. Compute the Q_1/Q_{10} ratio. From step 1 this is $2.94/6.68 = 0.44$.
3. Determine the permissible minimum base flow. Use the C_i value of 1.08 as determined, and table 21.4 to obtain the base flow value of 1.20 c.s.m.
4. Determine the net average discharge through the principal spillway. The maximum release rate for this situation has been assumed to be 10 c.s.m., and the average release rate is estimated to be 70 percent of the maximum, or 7 c.s.m. To get the net release rate, subtract the base flow inflow of 1.2 c.s.m. from the 7 c.s.m., giving a net discharge of 5.8 c.s.m. through the principal spillway.
5. Determine minimum floodwater retarding storage. Enter Figure 3 with a ratio of $Q_1/Q_{10} = 0.40$ which is the closest ratio to that determined in step 2, a T_c of 2.0 hours, and Q_{10} of 6.68 inches. Note that Figure 3 covers a range in T_c from 0.1 to 9.0 hours. Figure 3 gives a value of 4.60 inches of retarding storage for a

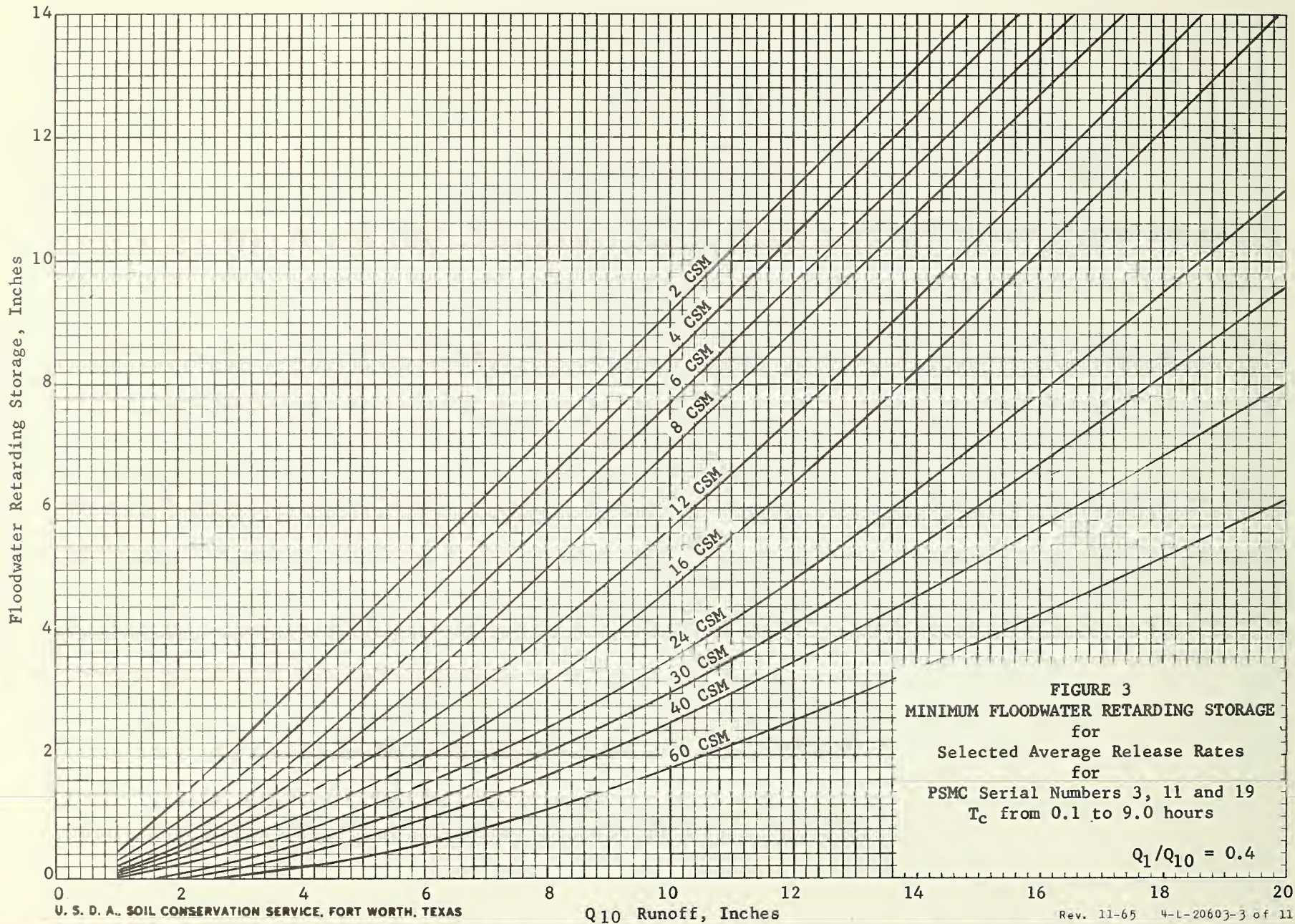
net release of 5.8 c.s.m. Then enter Figure 4 with the ratio of $Q_1/Q_{10} = 0.50$ and find the value of 4.50 inches of storage. By interpolation for a $Q_1/Q_{10} = 0.44$ the minimum retarding storage would be 4.54 inches.

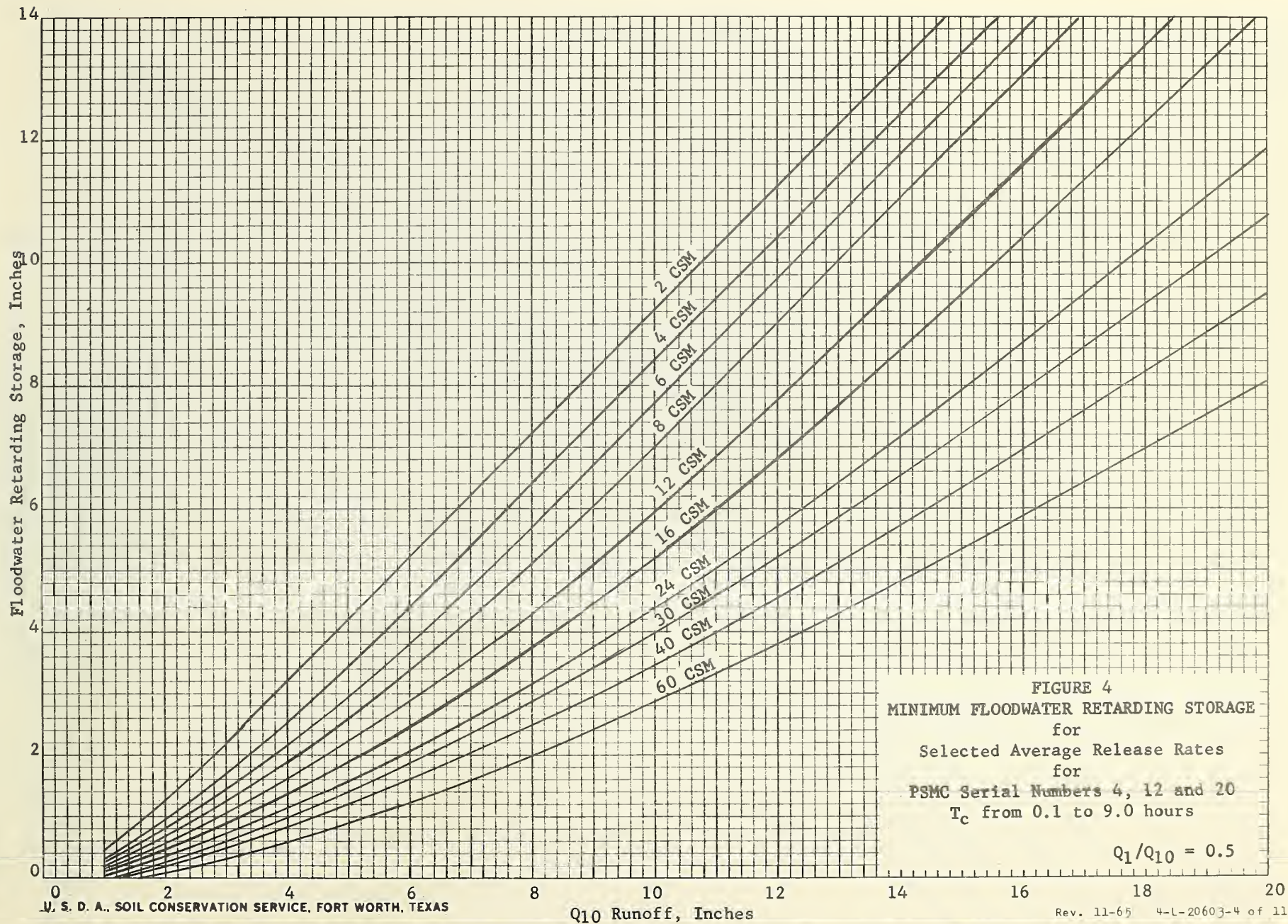
Figures 1 to 8, inclusive, were developed for T_c 's of 9 hours or less. When a greater T_c is to be used, it is suggested that the PSMC be routed.

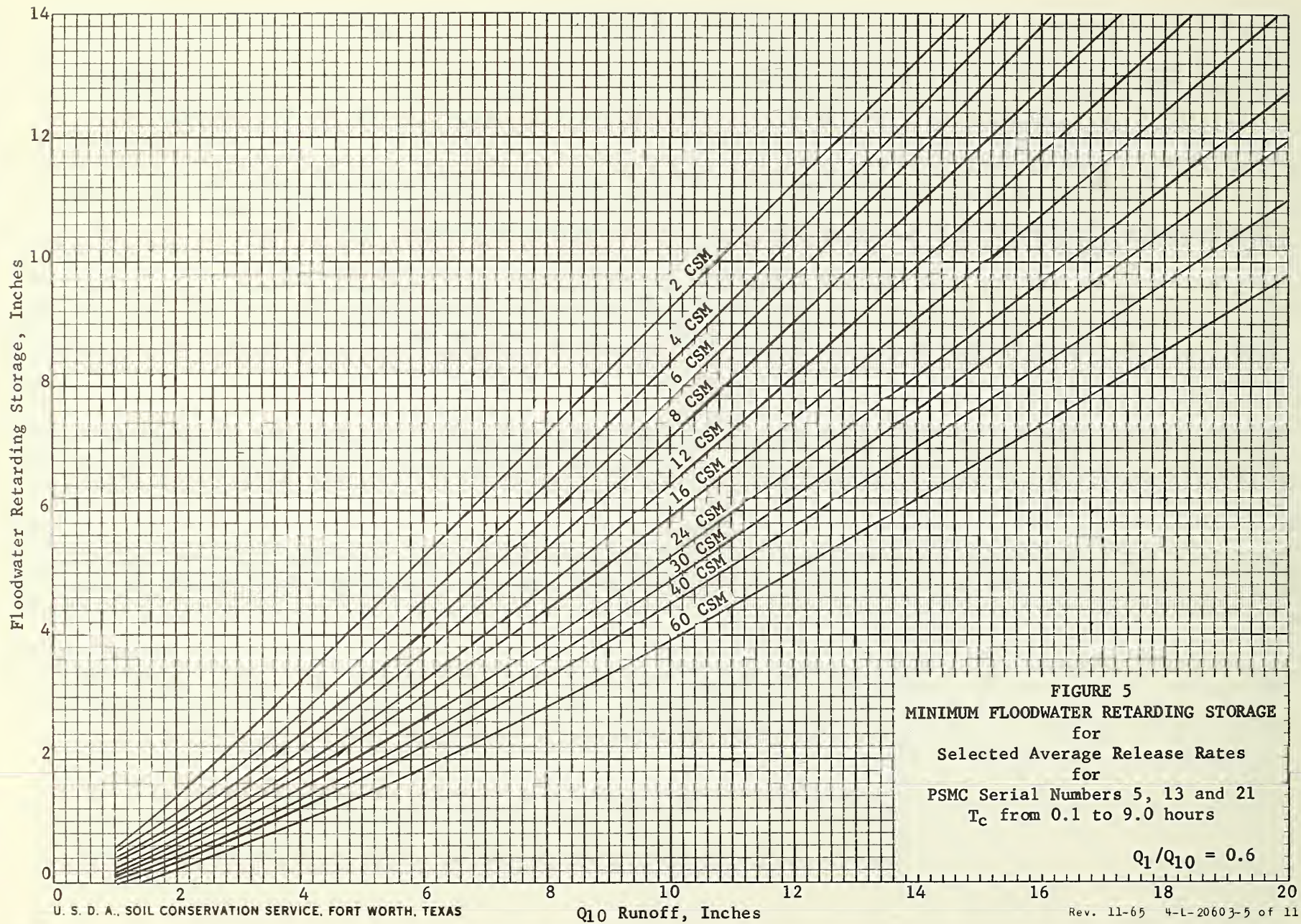
Storage requirements for various release rates that should be considered in conjunction with various downstream channel and flood plain situations can be quickly estimated by this method.

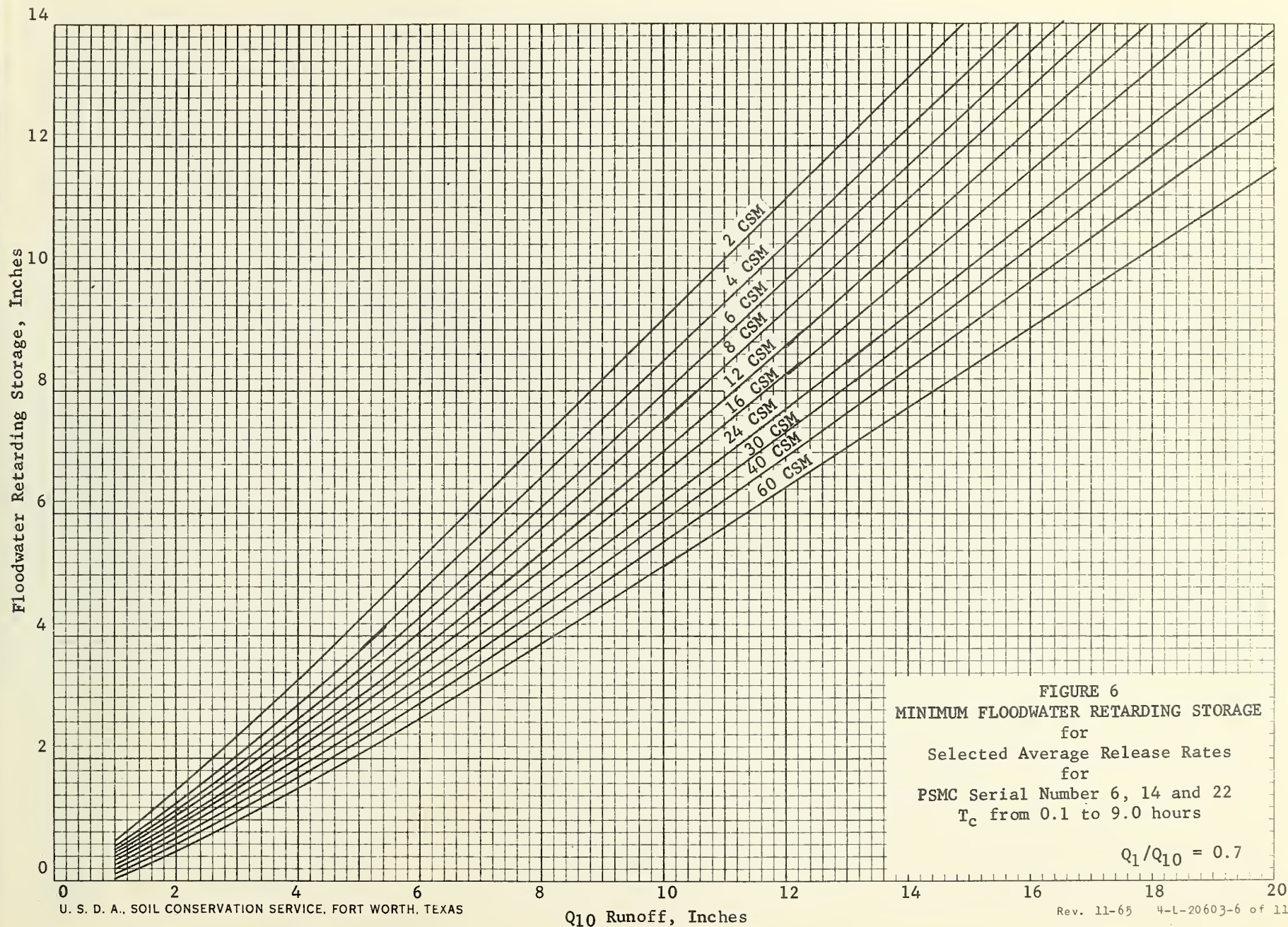












Floodwater Retarding Storage, Inches

